SEE Test Report V3.0<br>Heavy ion SEE test of MFP0507S from Interpoint Anthony B. Sanders ${ }^{1}$, Hak S. Kim ${ }^{2}$, Anthony M. Phan² Christina Seidleck ${ }^{2}$<br>${ }^{1}$ NASA GSFC<br>${ }^{2}$ MEI Technologies

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## I. Introduction

This study was undertaken to determine the susceptibility of the MFP0507, Single DC/DC Converters, for transient interruptions in the output signal and for destructive events such as gate rupture and burnout induced by exposing it to a heavy ion beam at the Radiation Effects Facility at The Cyclotron Institute located on the campus of Texas A\&M University. This test was performed for the investigation of radiation susceptibility of transient events and destructive events for Crane Interpoint. This work is in conjunction with the NASA Electronics Parts and Packaging (NEPP) Program. NEPP is a HQ sponsored program that seeks to find new developments that will benefit NASA.

The Interpoint MFP0507S is a single output non isolated point of load converter. The MFP will produce any output voltage from 0.8 VDC to 3.3 VDC . The rated output current is 7 Amps at 0.8 V and 5 Amps at 3.3 V . Input voltage range for the MFP is from 3.3 V to 6 V , however the selected output voltage should not exceed $80 \%$ of the input voltage. Any one of four precision output voltage set points can be selected by the combination of open or grounding of the two trim pins. Maximum output power of 16.5 W is with output set for 3.3 V and 5 A . Maximum output power with the output voltage set for 0.8 V and 7 Amp is 5.6 W . They are best suited for high reliability and high radiation assurance requirements with an LET of $80 \mathrm{MeV} \mathrm{cm}{ }^{2} / \mathrm{mg}$ for SEU. This document serves as a Test Plan intended to supplement any governing standards, for conducting and recording SEU on the MFP0507S due to several heavy ion species ( $\mathrm{Z} \geq 2$ ).

## II. Devices Tested

The sample size of Device Under Test (DUT) for testing was four. Each device was exposed to the radiation beam and the results were compared for verification. For the MFP0507S, the test samples code markings for DUT1 is SN-0077, .8V output; DUT2 SN-0078, .8V output; DUT3 SN-0082, 3.3V output; \& DUT4 SN-0083, 3.3V output. The device is packaged in a 10-pin lead metal can package. The device was prepped for test by delidding.

The MFP Series ${ }^{\text {TM }}$ of DC/DC converters does not require any external components to achieve all specified performance levels. They are a high-reliability, high-efficiency point of load converter for use with a 3.3 VDC input bus or a 5 VDC input bus. The

MFP0507S model has the flexibility to be set for any output voltage from 0.64 VDC to 3.5 VDC. The converter operates from an input of 3.0 to 6.0 VIN with an undervoltage shutdown at 2.75 V , an overvoltage shutdown of 8.5 V and up to a 15 V transient for up to 1 second. The non-isolated, feature-rich MFP uses a Buck converter design with synchronous rectification. The design allows the unit to operate synchronously to no output load, ensuring high efficiency at the lightest loads without switching off the synchronous devices. Important features include a solid state switch, inrush current limiting, and synchronization with an external system clock and the ability to current share allowing multiple devices to supply a common load.

The MFP includes an internal housekeeping supply that is active at inputs as low as 2 VDC and provides a boosted and regulated voltage supply for internal use. This internal supply is one of the reasons that this product can provide full power at very high efficiency at input voltages as low as 3 VDC. No external power source or external bias is required.

## III. Test Facility

Facility: Texas A\&M Cyclotron Radiation Effects Facility, $15 \mathrm{MeV} / \mathrm{u}$ beams
Flux: $\quad 1.23 \times 10^{2}$ to $1.20 \times 10^{5}$ particles $/ \mathrm{cm}^{2} / \mathrm{s}$.
Fluence: For destructive events, all tests were ran to $1 \times 10^{7} \mathrm{p} / \mathrm{cm}^{2}$ or until destructive events occurred
For non destructive events, all tests were ran to $1 \times 10^{6} \mathrm{p} / \mathrm{cm}^{2}$ or until a sufficient (>100) number of transient events occurred.

The ions and LET values used for these tests were Xe, Ta, \& Au.

## IV. Test Conditions and Error Modes

Test Temperature: Room Temperature
Bias conditions
$\mathrm{V}_{\text {in }}=6 \mathrm{~V}, \mathrm{~V}_{\text {out }}=.8 \mathrm{~V} \& 3.3 \mathrm{~V}$
See Figure 2 for detailed conditions

Table 1: Test conditions

|  | Vsupply <br> (V) | Isupply <br> $\mathbf{( A )}$ | Vin <br> (V) | Loading <br> $\mathbf{\%}$ |
| :---: | :---: | :---: | :---: | :---: |
| DUT 1 | +.8 V | .121 | 6 V | 0 |
| DUT 1 | +.8 V | .445 | 6 V | 30 |
| DUT 1 | +.8 V | .685 | 6 V | 50 |
| DUT 1 | +.8 V | .947 | 6 V | 70 |
| DUT 1 | +.8 V | 1.38 | 6 V | 100 |
| DUT 2 | +3.3 V | .117 | 6 V | 0 |
| DUT 2 | +3.3 V | .997 | 6 V | 30 |
| DUT 2 | +3.3 V | 1.60 | 6 V | 50 |
| DUT 2 | +3.3 V | 2.22 | 6 V | 70 |
| DUT 2 | +3.3 V | 3.17 | 6 V | 100 |
| DUT 3 | +.8 V | .120 | 6 V | 0 |
| DUT 3 | +.8 V | .440 | 6 V | 30 |
| DUT 3 | +.8 V | .680 | 6 V | 50 |
| DUT 3 | +.8 V | .941 | 6 V | 70 |
| DUT 3 | +.8 V | 1.375 | 6 V | 100 |
| DUT 4 | +3.3 V | .122 | 6 V | 0 |
| DUT 4 | +3.3 V | .999 | 6 V | 30 |
| DUT 4 | +3.3 V | 1.60 | 6 V | 50 |
| DUT 4 | +3.3 V | 2.22 | 6 V | 70 |
| DUT 4 | +3.3 V | 3.17 | 6 V | 100 |

PARAMETERS OF INTEREST: Power supply currents, output voltage
SEE Conditions: SEL, SEGR, SET

## V. Test Methods

The block diagram, as shown in Figure 1, for the DC-DC Converters contains a power supply for +/- input voltages, an electronic load, a DUT board for the test circuitry and devices, a computer for GPIB control of measurement equipment, and a digital scope to capture any output anomalies, and after the desired voltage input is applied, each of the two device outputs will display on the digital scope, which is set to trigger on voltages that are above or below a predetermined threshold (set to 250 mV ). Each device output was tested one after each other.

Table 1, shows the test conditions where tests were conducted for an input nominal voltage of 6 V with and without loading and also with loading conditions of $30,50,70$, and $100 \%$ loading with both $.8 \mathrm{~V} \& 3.3 \mathrm{~V}$ outputs. Figure 1 also shows the test schematic circuit of the MFP0507S and Figure 2 shows the device exposed for ion beams at TAMU.

## VI. Test Performance

- Destructive test at high LET ( $>85 \mathrm{MeVcm}^{2} / \mathrm{mg}$ ) on 4 parts up to a fluence of $10^{7}$ \#/cm ${ }^{2}$.
- SET test on 4 parts for at least 3 LET values (starting from lowest LET) for each device output and each condition described in Table 1.


Figure 1. Overall Block Diagram and Schematic for the testing of the MFP0507S


Figure 2. MFP0507S device exposed for ion beam test at TAMU

## VII. Test Results

Detailed test results are shown in Table 2 below. The devices were exposed from a fluence of $1.00 \times 10^{3}$ to $1.00 \times 10^{7}$ particles $/ \mathrm{cm}^{2}$ of the Xenon, Tantalum, and Gold ion beams. Observations for destructive and non-destructive events were for energies up to the maximum LET of $85.4 \mathrm{MeV}-\mathrm{cm}^{2} / \mathrm{mg}$ at normal angle of incidence. There were no destructive events observed for the MFP0507S, but the device was sensitive to SETs and did experience transient events with larger transients occurring at the .8 V output greater than 2 V and approximately 200us for worse case width duration shown in Charts $1 \& 2$. This large spike may need to be mitigated with using the appropriate LC filtering circuitry in conjunction with this DC-DC converter. The 3.3 V output transients were $<500 \mathrm{mV}$ and 100 us for worse case width duration shown in Charts $3 \& 4$. The tests were run with an input of 6 V with .8 V and 3.3 V output configurations at $30 \%, 50 \%, 70 \%$, and $100 \%$ loading conditions. Charts $5 \& 6$ show typical histograms of amplitude using the absolute values attained and Chart 7 shows the SET cross sections observed. In general most SETs were small for the 3.3 V output which is the common use for designers for space flight applications; therefore this device is suitable for space applications.


Charts 1\&2: Worse Case Transients of approx 1.74V and 200us with .8V Output


Charts 3: Typical Transient of appox 200 mV and 100 us with .8 V Output


Charts 4: Typical Transient of approx 800mV Peak-to-Peak and 200us with 3.3V Output


Chart 5: MFP0507S Amplitude Histogram for 3.3V input


Chart 6: MFP0507S Amplitude Histogram for 0.8V input


Chart 7: MFP0507S SET Cross Sections

Table 2: MFP0507S Data Collected at TAMU

| Run\# | \# | OUT | $\begin{aligned} & \text { IN } \\ & (\mathrm{V}) \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Trig } \\ & \mathrm{mV} \end{aligned}$ | Current(A) | Ion | Energy | LET | LET(eff) | angle | Flux | Fluence $_{\text {eff }}$ | SET | SEL | $\sigma_{\text {seu }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 77 | 0.8 V | 6 | 120 | 0.121 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 1.10E+04 | $2.76 \mathrm{E}+05$ | 97 | 0 | 8.13E-04 |
| 2 | 77 | 0.8 V | 6 | 120 | 0.121 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $8.81 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 90 | 0 | 9.39E-04 |
| 3 | 77 | 0.8 V | 6 | 120 | 0.123 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $9.28 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 99 | 0 | $1.06 \mathrm{E}-03$ |
| 4 | 77 | 0.8 V | 6 | 120 | 0.445 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $8.46 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 195 | 0 | 2.14E-03 |
| 5 | 77 | 0.8 V | 6 | 120 | 0.445 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 8.07E+02 | 9.97E+04 | 176 | 0 | $1.95 \mathrm{E}-03$ |
| 6 | 77 | 0.8 V | 6 | 120 | 0.685 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $8.64 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 196 | 0 | 2.16E-03 |
| 7 | 77 | 0.8 V | 6 | 120 | 0.685 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 7.77E+02 | $1.00 \mathrm{E}+05$ | 194 | 0 | $2.08 \mathrm{E}-03$ |
| 8 | 77 | 0.8 V | 6 | 120 | 0.947 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 7.62E+02 | $1.00 \mathrm{E}+05$ | 211 | 0 | $2.29 \mathrm{E}-03$ |
| 9 | 77 | 0.8 V | 6 | 120 | 0.947 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 7.49E+02 | $9.98 \mathrm{E}+04$ | 208 | 0 | $2.32 \mathrm{E}-03$ |
| 10 | 77 | 0.8 V | 6 | 120 | 1.38 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $7.43 \mathrm{E}+02$ | $9.99 \mathrm{E}+04$ | 201 | 0 | $2.14 \mathrm{E}-03$ |
| 11 | 77 | 0.8 V | 6 | 120 | 1.38 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 7.14E+02 | $9.99 \mathrm{E}+04$ | 180 | 0 | $1.93 \mathrm{E}-03$ |
| 12 | 82 | 3.3 V | 6 | 120 | 0.117 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 6.15E+02 | $1.00 \mathrm{E}+05$ | 125 | 0 | 1.33E-03 |
| 13 | 82 | 3.3 V | 6 | 120 | 0.117 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $6.14 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 157 | 0 | $1.61 \mathrm{E}-03$ |
| 14 | 82 | 3.3 V | 6 | 120 | 0.997 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $5.92 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 160 | 0 | $1.72 \mathrm{E}-03$ |
| 15 | 82 | 3.3 V | 6 | 120 | 0.997 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $5.75 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 185 | 0 | $1.97 \mathrm{E}-03$ |
| 16 | 82 | 3.3 V | 6 | 120 | 1.6 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 6.15E+02 | $9.99 \mathrm{E}+04$ | 184 | 0 | 2.01E-03 |
| 17 | 82 | 3.3 V | 6 | 120 | 1.6 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $6.08 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 167 | 0 | $1.76 \mathrm{E}-03$ |
| 18 | 82 | 3.3 V | 6 | 120 | 2.22 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $5.84 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 156 | 0 | $1.62 \mathrm{E}-03$ |
| 19 | 82 | 3.3 V | 6 | 120 | 2.22 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $5.69 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 158 | 0 | 1.67E-03 |
| 20 | 82 | 3.3 V | 6 | 120 | 3.17 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $5.63 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 153 | 0 | 1.59E-03 |
| 21 | 78 | 3.3 V | 6 | 120 | 3.17 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 5.47E+02 | $9.98 \mathrm{E}+04$ | 166 | 0 | $1.73 \mathrm{E}-03$ |
| 22 | 78 | 0.8 V | 6 | 120 | 0.12 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.52 \mathrm{E}+02$ | $9.99 \mathrm{E}+04$ | 117 | 0 | $1.22 \mathrm{E}-03$ |
| 23 | 78 | 0.8 V | 6 | 120 | 0.44 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.42 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 229 | 0 | $2.43 \mathrm{E}-03$ |
| 24 | 78 | 0.8 V | 6 | 120 | 0.68 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.38 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 239 | 0 | $2.45 \mathrm{E}-03$ |
| 25 | 78 | 0.8 V | 6 | 120 | 0.941 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.24 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 221 | 0 | $2.27 \mathrm{E}-03$ |
| 26 | 78 | 0.8 V | 6 | 120 | 1.375 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.27 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 231 | 0 | $2.44 \mathrm{E}-03$ |
| 27 | 83 | 3.3 V | 6 | 120 | 0.122 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.10 \mathrm{E}+02$ | $9.99 \mathrm{E}+04$ | 112 | 0 | $1.13 \mathrm{E}-03$ |
| 28 | 83 | 3.3 V | 6 | 120 | 0.999 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.13 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 146 | 0 | $1.52 \mathrm{E}-03$ |
| 29 | 83 | 3.3 V | 6 | 120 | 1.6 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | $4.13 \mathrm{E}+02$ | $9.99 \mathrm{E}+04$ | 138 | 0 | $1.42 \mathrm{E}-03$ |
| 30 | 83 | 3.3 V | 6 | 120 | 2.22 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 3.87E+02 | $1.00 \mathrm{E}+05$ | 141 | 0 | $1.46 \mathrm{E}-03$ |
| 31 | 83 | 3.3 V | 6 | 120 | 3.16 | Xe-15 | 1512 | 51.5 | 51.5 | 0 | 3.87E+02 | $9.99 \mathrm{E}+04$ | 150 | 0 | $1.52 \mathrm{E}-03$ |
| 32 | 83 | 3.3 V | 6 | 120 | 0.124 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $1.40 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 153 | 0 | $1.84 \mathrm{E}-03$ |
| 33 | 83 | 3.3 V | 6 | 120 | 1 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $1.34 \mathrm{E}+03$ | $9.95 \mathrm{E}+04$ | 161 | 0 | $1.83 \mathrm{E}-03$ |
| 34 | 83 | 3.3 V | 6 | 120 | 1.6 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $1.23 \mathrm{E}+02$ | $9.95 \mathrm{E}+04$ | 169 | 0 | $2.05 \mathrm{E}-03$ |
| 35 | 83 | 3.3 V | 6 | 120 | 2.22 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $1.23 \mathrm{E}+03$ | $9.95 \mathrm{E}+04$ | 197 | 0 | $2.36 \mathrm{E}-03$ |
| 36 | 83 | 3.3 V | 6 | 120 | 3.17 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $1.00 \mathrm{E}+03$ | $1.20 \mathrm{E}+05$ | 172 | 0 | $1.73 \mathrm{E}-03$ |
| 37 | 78 | 0.8 V | 6 | 120 | 0.122 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $9.85 \mathrm{E}+02$ | $9.98 \mathrm{E}+04$ | 82 | 0 | $8.62 \mathrm{E}-04$ |
| 38 | 78 | 0.8 V | 6 | 120 | 0.443 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 8.94E+02 | 9.97E+04 | 119 | 0 | $1.26 \mathrm{E}-03$ |
| 39 | 78 | 0.8 V | 6 | 120 | 0.683 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $8.34 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 141 | 0 | 1.51E-03 |
| 40 | 78 | 0.8 V | 6 | 120 | 0.943 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $8.72 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 149 | 0 | $1.60 \mathrm{E}-03$ |
| 41 | 78 | 0.8 V | 6 | 120 | 1.37 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 7.31E+02 | $1.00 \mathrm{E}+05$ | 189 | 0 | 2.04E-03 |
| 42 | 77 | 0.8 V | 6 | 120 | 0.126 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 7.95E+02 | $1.00 \mathrm{E}+05$ | 56 | 0 | 5.70E-04 |
| 43 | 77 | 0.8 V | 6 | 120 | 0.447 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $7.79 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 94 | 0 | $9.90 \mathrm{E}-04$ |
| 44 | 77 | 0.8 V | 6 | 120 | 0.688 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 7.64E+02 | $1.00 \mathrm{E}+05$ | 122 | 0 | $1.27 \mathrm{E}-03$ |
| 45 | 77 | 0.8 V | 6 | 120 | 0.951 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 7.19E+02 | $1.00 \mathrm{E}+05$ | 150 | 0 | $1.57 \mathrm{E}-03$ |
| 46 | 77 | 0.8 V | 6 | 120 | 1.39 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 7.07E+02 | $9.98 \mathrm{E}+04$ | 158 | 0 | $1.66 \mathrm{E}-03$ |
| 47 | 82 | 3.3 V | 6 | 120 | 0.123 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $6.74 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 196 | 0 | $2.07 \mathrm{E}-03$ |

Table 2: MFP0507S Data Collected at TAMU (Cont.)

| Run\# | \# | OUT | $\begin{aligned} & \text { IN } \\ & (\mathrm{V}) \end{aligned}$ | Trig mV | Current(A) | Ion | Energy | LET | LET(eff) | angle | Flux | Fluence $_{\text {eff }}$ | SET | SEL | $\sigma_{\text {seu }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 48 | 82 | 3.3 V | 6 | 120 | 1 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 6.69E+02 | $1.00 \mathrm{E}+05$ | 196 | 0 | 2.12E-03 |
| 49 | 82 | 3.3 V | 6 | 120 | 1.6 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $6.28 \mathrm{E}+02$ | $1.00 \mathrm{E}+05$ | 217 | 0 | $2.30 \mathrm{E}-03$ |
| 50 | 82 | 3.3 V | 6 | 120 | 2.23 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | $6.18 \mathrm{E}+02$ | 9.99E+04 | 199 | 0 | $2.15 \mathrm{E}-03$ |
| 51 | 82 | 3.3 V | 6 | 120 | 3.18 | Ta-15 | 2076 | 77.3 | 77.3 | 0 | 6.13E+02 | 9.99E+04 | 194 | 0 | $2.09 \mathrm{E}-03$ |
| 52 | 82 | 3.3 V | 6 | 120 | 0.13 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.28 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 164 | 0 | $1.81 \mathrm{E}-03$ |
| 53 | 82 | 3.3 V | 6 | 120 | 1.01 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.18E+03 | 9.97E+04 | 208 | 0 | $2.59 \mathrm{E}-03$ |
| 54 | 82 | 3.3 V | 6 | 120 | 1.61 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.22E+03 | $9.96 \mathrm{E}+04$ | 189 | 0 | $2.24 \mathrm{E}-03$ |
| 55 | 82 | 3.3 V | 6 | 120 | 2.23 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.12E+03 | $1.00 \mathrm{E}+05$ | 216 | 0 | $2.64 \mathrm{E}-03$ |
| 56 | 82 | 3.3 V | 6 | 120 | 3.19 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.13 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 192 | 0 | $2.30 \mathrm{E}-03$ |
| 57 | 77 | 0.8V | 6 | 120 | 0.129 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 9.11E+02 | $1.00 \mathrm{E}+05$ | 161 | 0 | $1.73 \mathrm{E}-03$ |
| 58 | 77 | 0.8 V | 6 | 120 | 0.415 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 9.61E+02 | 9.98E+04 | 191 | 0 | $2.07 \mathrm{E}-03$ |
| 59 | 77 | 0.8V | 6 | 120 | 0.691 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.02 \mathrm{E}+03$ | $9.96 \mathrm{E}+04$ | 193 | 0 | 2.13E-03 |
| 60 | 77 | 0.8 V | 6 | 120 | 0.955 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.04 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 205 | 0 | $2.37 \mathrm{E}-03$ |
| 61 | 77 | 0.8V | 6 | 120 | 1.39 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.06 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 187 | 0 | $2.22 \mathrm{E}-03$ |
| 62 | 78 | 0.8V | 6 | 120 | 0.124 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.12E+03 | $1.00 \mathrm{E}+05$ | 198 | 0 | $2.36 \mathrm{E}-03$ |
| 63 | 78 | 0.8V | 6 | 120 | 0.446 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.16 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 188 | 0 | $2.26 \mathrm{E}-03$ |
| 64 | 78 | 0.8 V | 6 | 120 | 0.686 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.12E+03 | $1.00 \mathrm{E}+05$ | 193 | 0 | $2.27 \mathrm{E}-03$ |
| 65 | 78 | 0.8V | 6 | 120 | 0.949 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.16E+03 | 1.00E+05 | 204 | 0 | $2.49 \mathrm{E}-03$ |
| 66 | 78 | 0.8V | 6 | 120 | 1.39 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.15E+03 | $1.00 \mathrm{E}+05$ | 188 | 0 | $2.29 \mathrm{E}-03$ |
| 67 | 83 | 3.3V | 6 | 120 | 0.132 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.18 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 134 | 0 | $1.44 \mathrm{E}-03$ |
| 68 | 83 | 3.3V | 6 | 120 | 1.01 | Au-15 | 2247 | 85.4 | 85.4 | 0 | $1.15 \mathrm{E}+03$ | $1.00 \mathrm{E}+05$ | 140 | 0 | $1.60 \mathrm{E}-03$ |
| 69 | 83 | 3.3 V | 6 | 120 | 1.61 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.13E+03 | $1.00 \mathrm{E}+05$ | 161 | 0 | 1.83E-03 |
| 70 | 83 | 3.3V | 6 | 120 | 2.23 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.20E+03 | 9.98E+04 | 134 | 0 | 1.51E-03 |
| 71 | 83 | 3.3V | 6 | 120 | 3.18 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.17E+03 | $1.00 \mathrm{E}+05$ | 141 | 0 | $1.65 \mathrm{E}-03$ |
| 72 | 83 | 3.3 V | 6 | 120 | 3.18 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 5.55E+04 | $1.00 \mathrm{E}+07$ | 551 | 0 | 5.34E-04 |
| 73 | 83 | 3.3V | 6 | 120 | 3.35 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.09E+05 | 8.98E+06 | 238 | 0 | 3.57E-04 |
| 74 | 83 | 3.3 V | 6 | 120 | 3.46 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 1.37E+04 | $9.98 \mathrm{E}+06$ | 424 | 0 | 5.46E-04 |
| 75 | 83 | 3.3 V | 6 | 120 | 3.64 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 9.51E+04 | $1.00 \mathrm{E}+07$ | 425 | 0 | 5.45E-04 |
| 76 | 83 | 3.3 V | 6 | 120 | 3.8 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 8.23E+04 | 6.11E+06 | 184 | 0 | 3.68E-04 |
| 77 | 83 | 3.3 V | 6 | 120 | 3.8 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 8.21E+04 | 6.17E+06 | 275 | 0 | 5.55E-04 |
| 78 | 78 | 0.8V | 6 | 120 | 1.38 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 7.77E+04 | $1.00 \mathrm{E}+07$ | 520 | 0 | $6.30 \mathrm{E}-04$ |
| 79 | 78 | 0.8V | 6 | 120 | 1.52 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 8.31E+04 | $1.00 \mathrm{E}+07$ | 488 | 0 | 5.31E-04 |
| 80 | 78 | 0.8V | 6 | 120 | 1.61 | Au-15 | 2247 | 85.4 | 85.4 | 0 | 8.26E+04 | $1.00 \mathrm{E}+07$ | 491 | 0 | 5.33E-04 |

SEE Test Report V3.0_Addendum
Heavy ion SEE test of MFP0507S from Interpoint
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Test Date(s): January 21-23, 2011

## VIII. Addendum

This study was undertaken to determine the susceptibility of the MFP0507, Single DC/DC Converters, for transient interruptions in the output signal and for destructive events such as gate rupture and burnout induced by exposing it to a heavy ion beam at the Lawrence Berkeley Nuclear Laboratory (LBNL). Utilizing the Berkeley Accelerator Space Effects Facility (BASEF) this follow-on test was performed for the investigation of radiation susceptibility of transient events and destructive events for Crane Interpoint to determine the transient threshold for the device. This work is in conjunction with the NASA Electronics Parts and Packaging (NEPP) Program. NEPP is a HQ sponsored program that seeks to find new developments that will benefit NASA.

## IX. Test Facility

Facility: Lawrence Berkeley Nuclear Laboratory, $10 \mathrm{MeV} / \mathrm{u}$ beams
Flux: $\quad 5.14 \times 10^{4}$ to $7.43 \times 10^{4}$ particles $/ \mathrm{cm}^{2} / \mathrm{s}$.
Fluence: For destructive events, all tests were ran to $1 \times 10^{7} \mathrm{p} / \mathrm{cm}^{2}$ or until destructive events occurred
For non destructive events, all tests were ran to $1 \times 10^{7} \mathrm{p} / \mathrm{cm}^{2}$ or until a sufficient (>100) number of transient events occurred.

The ions and LET values used for these tests were Ne \& Ar.

## X. Test Conditions and Error Modes

## Test Temperature: <br> Bias conditions

Room Temperature
$\mathrm{V}_{\text {in }}=6 \mathrm{~V}, \mathrm{~V}_{\text {out }}=.8 \mathrm{~V} \& 3.3 \mathrm{~V}$
See Figure 2 for detailed conditions

## XI. Test Results

Detailed test results are shown in Table 3 below. The devices were exposed to a fluence of $1.00 \times 10^{7}$ particles $/ \mathrm{cm}^{2}$ of the Neon and Argon ion beams. Transients were observed down to Neon for both the 0.8 and 3.3 V devices, but only for the higher load. The 3.3V device triggered only with 5A load. One 0.8 V device showed upsets for loads of 3.5 A or higher, and the other did not show any upsets. The transient events were similar in magnitude as the previous test at Texas A\&M University Cyclotron.
Therefore we can conclude that the threshold is $\sim \mathrm{LET}_{\text {th }}$ of $3.49 \mathrm{MeV}-\mathrm{cm}^{2} / \mathrm{mg}$ at normal angle of incidence.


Chart 8: MFP0507S SET Cross Sections

Table 3: MFP0507S Data Collected at LBNL

| Run | Serial | $\begin{gathered} \text { OUT } \\ (\mathrm{V}) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { IN } \\ & (\mathrm{V}) \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Trig } \\ & (\mathrm{mV}) \end{aligned}$ | Current(A) | $\operatorname{Load}(\mathrm{A})$ | Ion | $\begin{aligned} & \mathrm{E} \\ & (\mathrm{MeV}) \end{aligned}$ | LET | $\begin{aligned} & \text { Eff } \\ & \text { LET } \end{aligned}$ | Angle | $\begin{aligned} & \text { Flux (cm-2. s- } \\ & \text { 1) } \end{aligned}$ | $\begin{aligned} & \text { Fluence }_{\text {eff }} \text { (cm- } \\ & \text { 2) } \end{aligned}$ | SETs | $\mathrm{S}_{\text {seu }}(\mathrm{cm} 2)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 77 | 0.8 | 6 | 210 | 0.127 | 0 | Ar | 400 | 9.7 | 9.7 | 0 | $5.50 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 9 | $9.00 \mathrm{E}-07$ |
| 2 | 77 | 0.8 | 6 | 210 | 0.451 | 2.12 | Ar | 400 | 9.7 | 9.7 | 0 | $5.52 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 23 | $2.30 \mathrm{E}-06$ |
| 3 | 77 | 0.8 | 6 | 210 | 0.695 | 3.53 | Ar | 400 | 9.7 | 9.7 | 0 | $5.79 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 55 | 5.50E-06 |
| 4 | 77 | 0.8 | 6 | 210 | 0.968 | 4.92 | Ar | 400 | 9.7 | 9.7 | 0 | $5.54 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 113 | $1.13 \mathrm{E}-05$ |
| 5 | 82 | 3.3 | 6 | 210 | 0.131 | 0 | Ar | 400 | 9.7 | 9.7 | 0 | $5.48 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 15 | 1.50E-06 |
| 6 | 82 | 3.3 | 6 | 120 | 1.066 | 1.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.55 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 15 | $1.50 \mathrm{E}-06$ |
| 7 | 82 | 3.3 | 6 | 120 | 1.77 | 2.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.30 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 22 | $2.20 \mathrm{E}-06$ |
| 8 | 82 | 3.3 | 6 | 120 | 2.52 | 3.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.50 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 38 | $3.80 \mathrm{E}-06$ |
| 9 | 82 | 3.3 | 6 | 120 | 4.2 | 5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.50 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 179 | $1.79 \mathrm{E}-05$ |
| 10 | 82 | 3.3 | 6 | 120 | 0.138 | 0 | Ne | 216 | 3.49 | 3.49 | 0 | $7.30 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 11 | 82 | 3.3 | 6 | 120 | 1.07 | 1.5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.13 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 12 | 82 | 3.3 | 6 | 120 | 1.79 | 2.5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.08 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 13 | 82 | 3.3 | 6 | 120 | 2.59 | 3.5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.42 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 14 | 82 | 3.3 | 6 | 120 | 4.21 | 5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.37 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 15 | $1.50 \mathrm{E}-06$ |
| 15 | 77 | 0.8 | 6 | 210 | 0.132 | 0 | Ne | 216 | 3.49 | 3.49 | 0 | $7.32 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | $1.00 \mathrm{E}-07$ |
| 16 | 77 | 0.8 | 6 | 210 | 0.454 | 2.12 | Ne | 216 | 3.49 | 3.49 | 0 | $7.40 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | $1.00 \mathrm{E}-07$ |
| 17 | 77 | 0.8 | 6 | 210 | 0.699 | 3.53 | Ne | 216 | 3.49 | 3.49 | 0 | $7.43 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 6 | $6.00 \mathrm{E}-07$ |
| 18 | 77 | 0.8 | 6 | 210 | 0.971 | 4.92 | Ne | 216 | 3.49 | 3.49 | 0 | $7.40 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 9 | $9.00 \mathrm{E}-07$ |
| 19 | 85 | 3.3 | 6 | 120 | 0.113 | 0 | Ne | 216 | 3.49 | 3.49 | 0 | $7.23 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 20 | 85 | 3.3 | 6 | 120 | 2.53 | 3.5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.05 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 21 | 85 | 3.3 | 6 | 120 | 4.07 | 5 | Ne | 216 | 3.49 | 3.49 | 0 | $7.17 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 15 | 1.50E-06 |
| 22 | 79 | 0.8 | 6 | 300 | 0.942 | 4.92 | Ne | 216 | 3.49 | 3.49 | 0 | $7.26 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | $0.00 \mathrm{E}+00$ |
| 23 | 79 | 0.8 | 6 | 300 | 0.112 | 0 | Ar | 400 | 9.7 | 9.7 | 0 | $5.35 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 13 | $1.30 \mathrm{E}-06$ |
| 24 | 79 | 0.8 | 6 | 300 | 0.436 | 2.12 | Ar | 400 | 9.7 | 9.7 | 0 | $5.59 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 20 | $2.00 \mathrm{E}-06$ |
| 25 | 79 | 0.8 | 6 | 300 | 0.683 | 3.53 | Ar | 400 | 9.7 | 9.7 | 0 | $5.54 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 27 | $2.70 \mathrm{E}-06$ |
| 26 | 79 | 0.8 | 6 | 300 | 0.961 | 4.92 | Ar | 400 | 9.7 | 9.7 | 0 | $5.38 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 77 | $7.70 \mathrm{E}-06$ |
| 27 | 85 | 3.3 | 6 | 200 | 0.113 | 0 | Ar | 400 | 9.7 | 9.7 | 0 | $5.38 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 22 | $2.20 \mathrm{E}-06$ |
| 28 | 85 | 3.3 | 6 | 200 | 1.048 | 1.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.14 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 53 | $5.30 \mathrm{E}-06$ |
| 29 | 85 | 3.3 | 6 | 200 | 1.754 | 2.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.45 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 53 | $5.30 \mathrm{E}-06$ |
| 30 | 85 | 3.3 | 6 | 200 | 2.58 | 3.5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.40 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 100 | $1.00 \mathrm{E}-05$ |
| 31 | 85 | 3.3 | 6 | 200 | 4.22 | 5 | Ar | 400 | 9.7 | 9.7 | 0 | $5.31 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 128 | $1.28 \mathrm{E}-05$ |

